

# LSST Structural Design

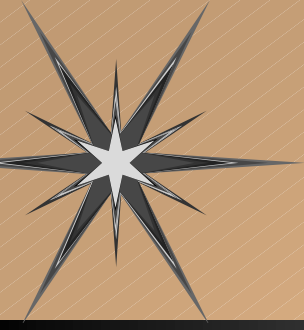
Warren Davison - Steward Observatory

Il Kweon Moon - Steward Observatory



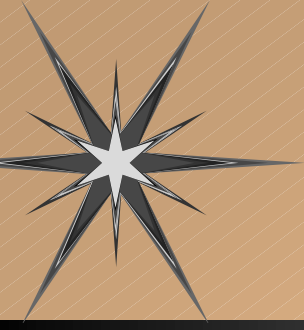
# Special LSST design considerations

- Unique optics and mass distribution
- Center of mass of the optics alone is near the vertex of the primary
- The center of mass of optics plus cells is near the rear of the primary
- Therefore the elevation axis structure is the primary mirror cell



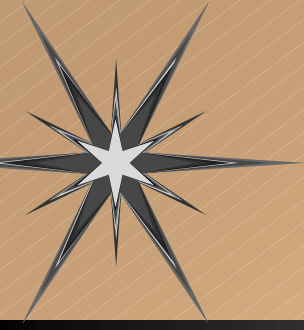
# Rationale for high stiffness

- Telescopes benefit from better structural stiffness and thus servo performance in many ways.
  - Tracking is better.
  - Wind rejection is better.
  - Pointing corrections are smaller.
  - Optics moving with gravity is reduced.
- High stiffness is worth the trouble.



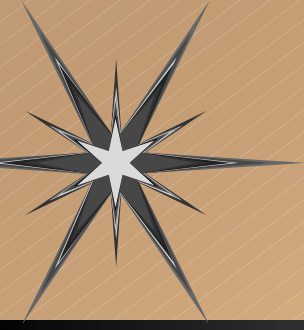
# Servo Performance Criteria

- Experience has shown an alt-az telescope with a 1 Hz servo bandwidth will track at about 0.15 arc-seconds rms.
- A good tracking servo performance goal is 2 Hz.
- Wind has significant power even up to 3 Hz.
- We need an Error Budget to do it right.
- We need servo analysis to do it right.



# Derived Structure Performance Criteria

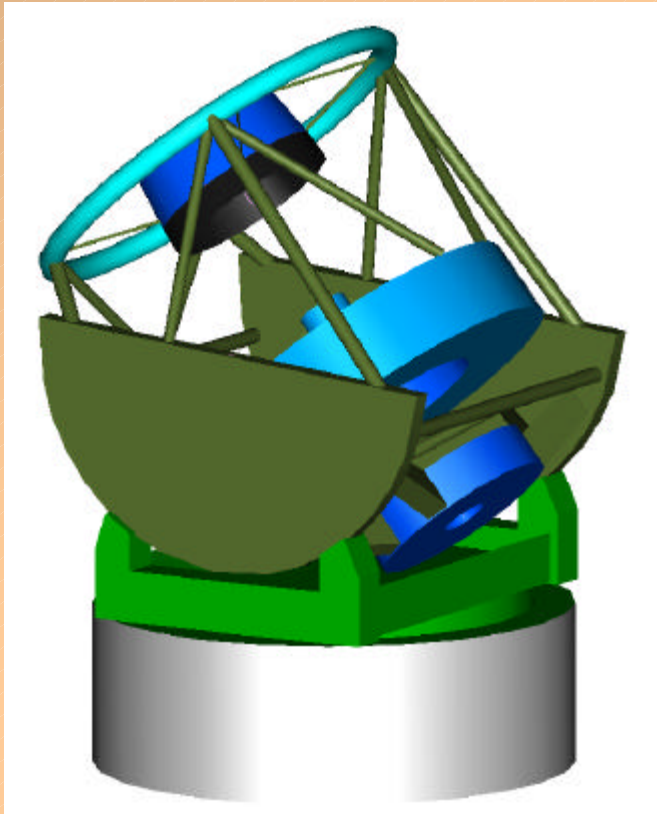
- Since the servo needs to be about 2 to 3 Hz. The structure needs a locked rotor resonant frequency of 4 times that or about 8 to 12 Hz.
- With the right design this is very realistic.
- Our preliminary design has a lowest frequency of 7.1 Hz which can easily be improved.
- We need to continue this effort.



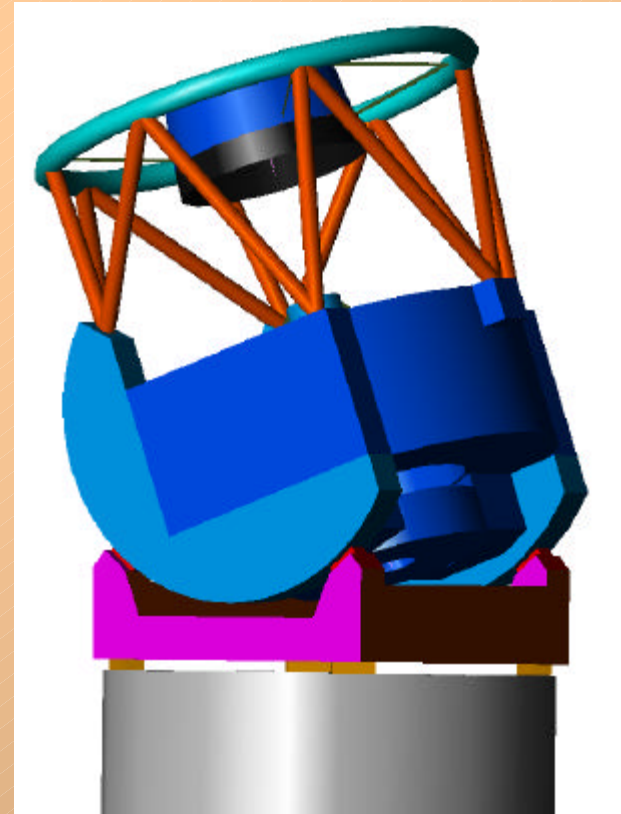
# Initial Evolution of Design

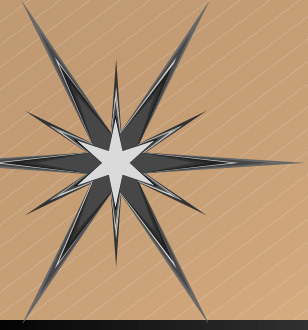


Concept



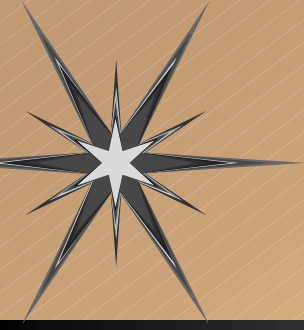
First Design





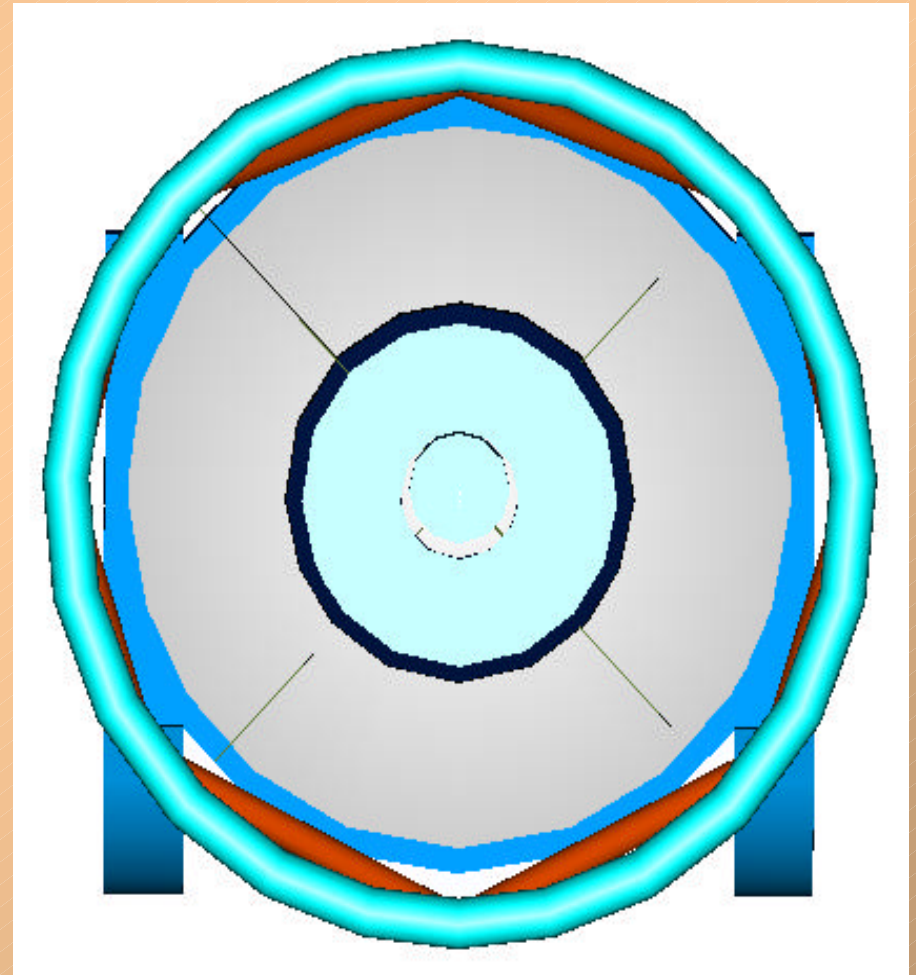
# Why C-Rings

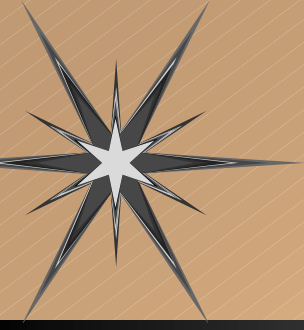
- The compliance of the mechanics depends on the square of their radius
- The bearings and drives of telescopes are usually made small to decrease their cost. Thus their compliance contribution is usually about 4 times the structure.
- Simply increasing the bearing surface and ring gear from 2m to 9m makes the same components 20 times stiffer which should double the frequency performance.



# Telescope Design Features

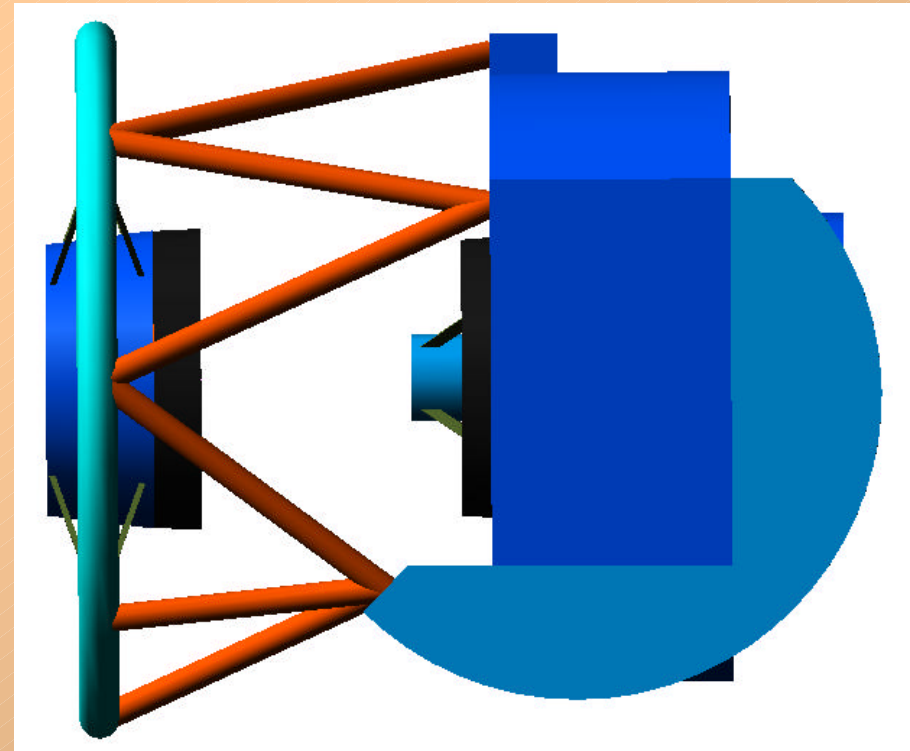
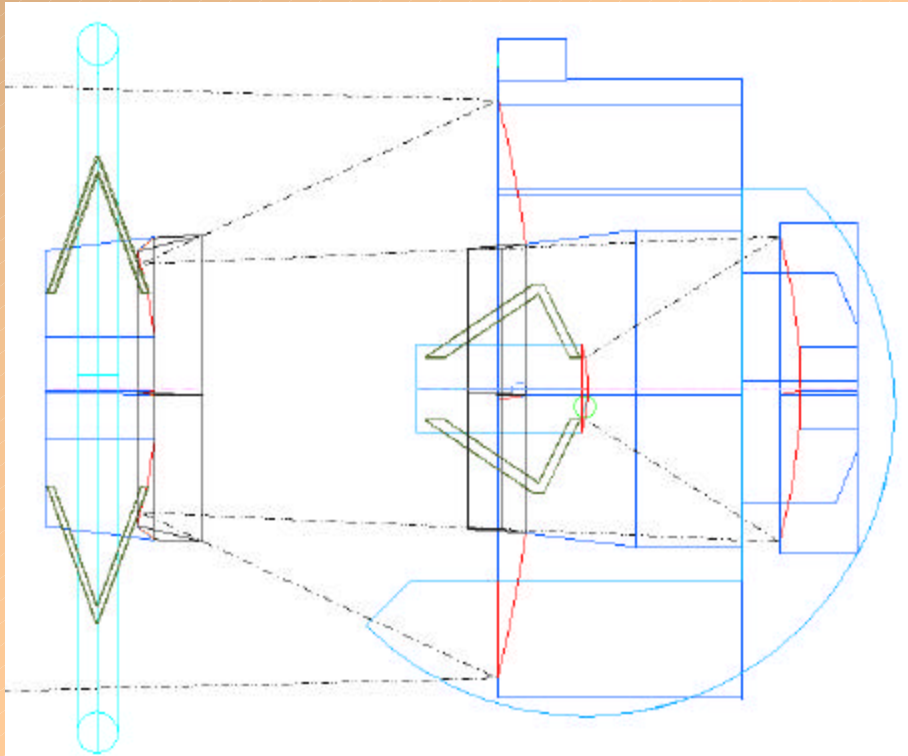
- Center to center distance of C-rings is 8m, glass diameter is 8.4.
- Primary mirror cell made an integral part of the structure.
- Top ring is largest diameter element.

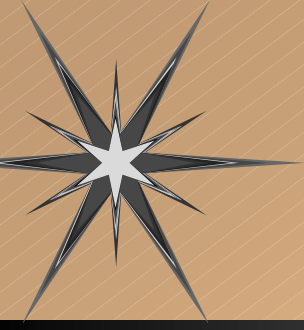




# Telescope Design Features

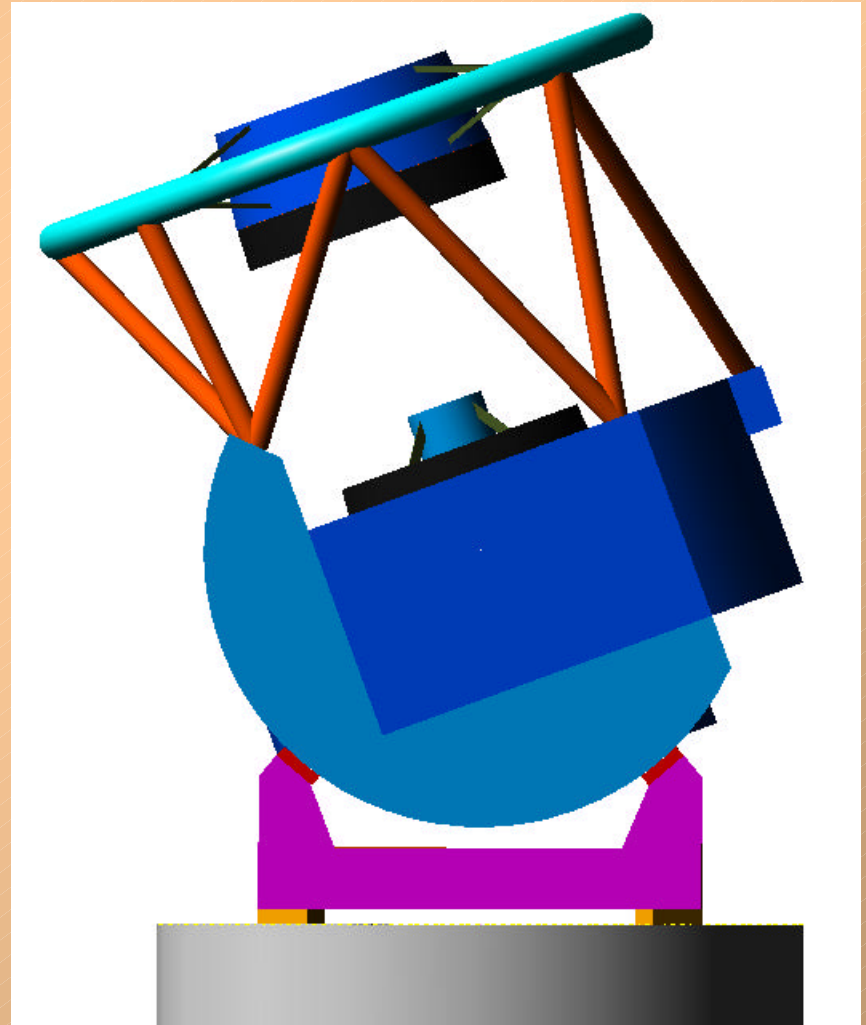
- Swing radius of 9.2m
- Optical axis and telescope axis are not coincident to achieve balance.

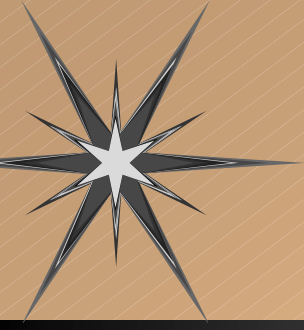




# Telescope Design Features

- ❑ Compact azimuth platform with the elevation bearings directly above azimuth bearings.
- ❑ Top of pier bearing surface 10.5 meters diameter.
- ❑ Lateral bearings on edges of C-rings.
- ❑ Center mechanical bearing or lateral bearing on side of azimuth bearing.

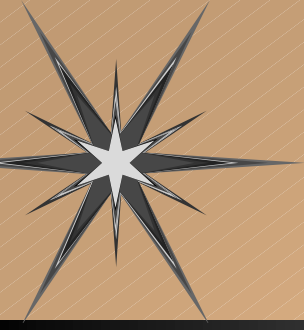




# LBT Design features

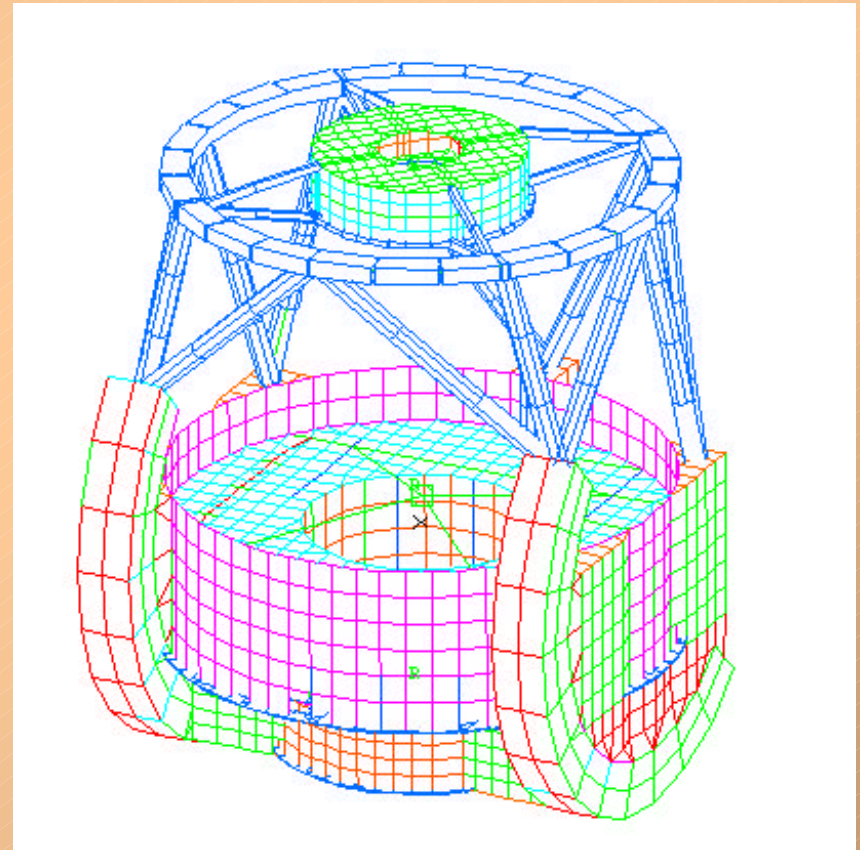
- Compact azimuth platform with the elevation bearings directly above azimuth bearings.
- Top of pier bearing surface 14 meters diameter.
- Lateral bearings on edges of C-rings.
- Center mechanical bearing

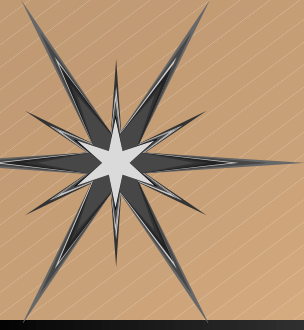




# FEA Telescope Model

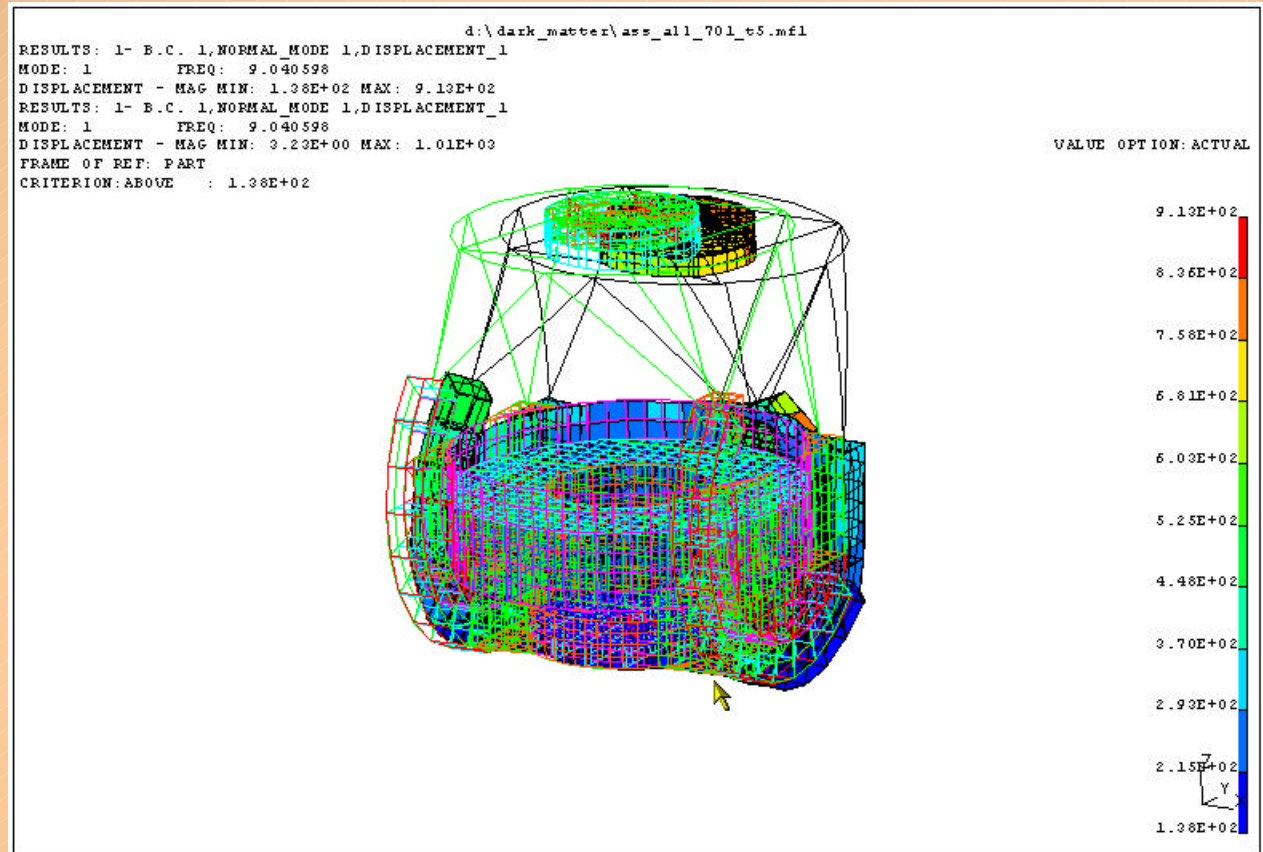
- The FEA model has 25,800 degrees of freedom.
- Total mass 232 tons.
- Total elevation mass 163 tons.
- Optics mass 23 tons
- Secondary assembly mass x tons.

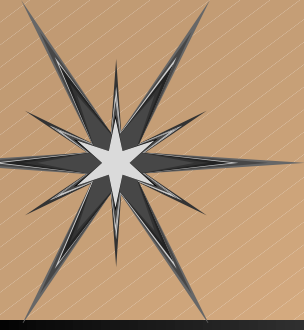




# Elevation Structure FEA

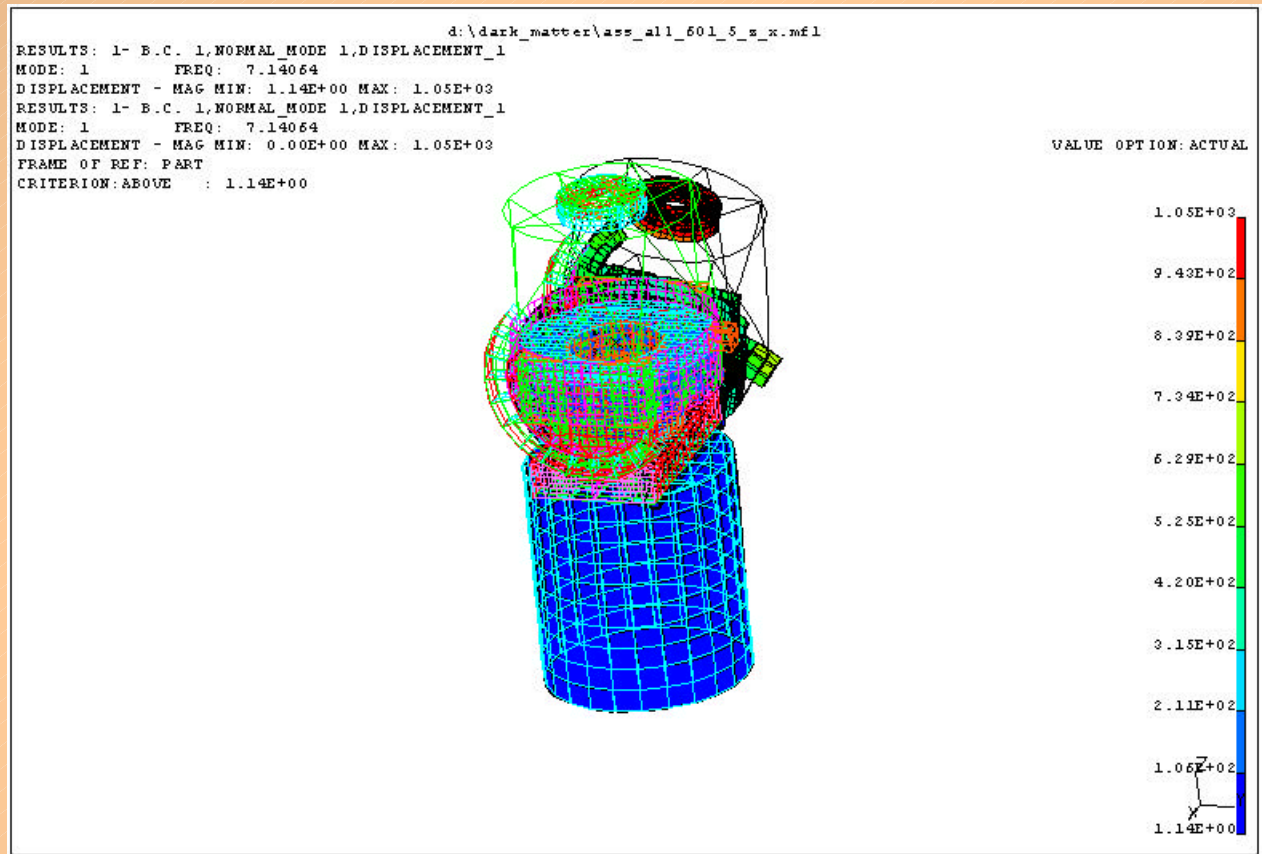
- First resonant frequency 9Hz  
– Elevation rocking mode.
- Can easily be improved by eliminating design error of front truss attachment

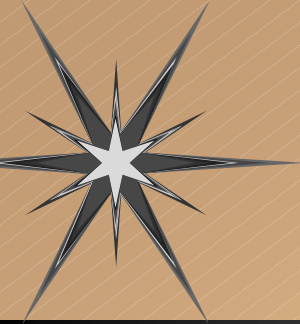




# First Telescope Resonance

- The First resonant frequency of the entire telescope is at 7.1 Hz.
- Elevation mode caused by a local deflection.

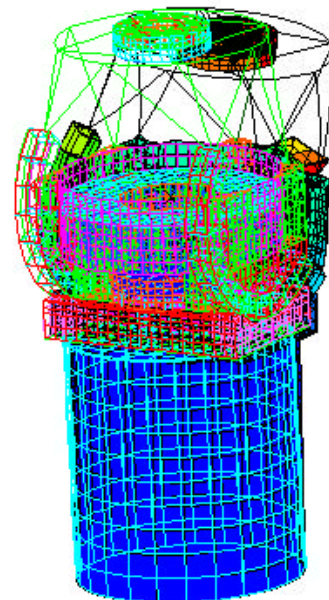




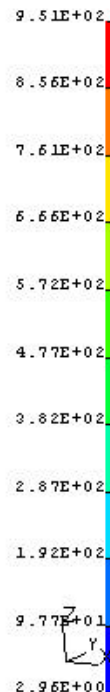
# Second Telescope Resonance

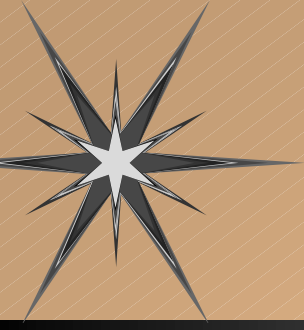
- Second mode 8.7Hz.

```
d:\dark_matter\ass_all_601_5_s_x.mfl
RESULTS: 2- B.C. 1,NORMAL_MODE 2,DISPLACEMENT_2
MODE: 2          FREQ: 8.704409
DISPLACEMENT - MAG MIN: 2.96E+00 MAX: 9.51E+02
RESULTS: 2- B.C. 1,NORMAL_MODE 2,DISPLACEMENT_2
MODE: 2          FREQ: 8.704409
DISPLACEMENT - MAG MIN: 0.00E+00 MAX: 1.01E+03
FRAME OF REF: PART
CRITERION: ABOVE : 2.96E+00
```



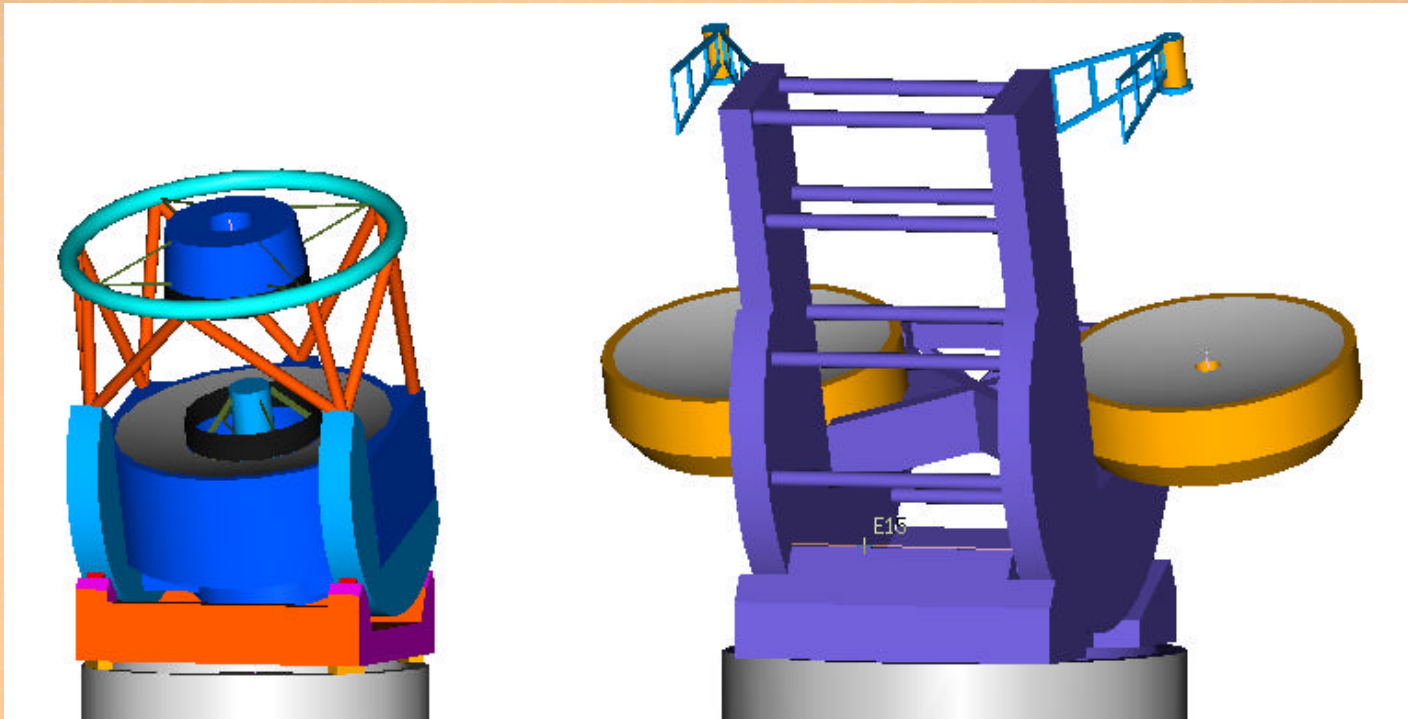
VALUE OPTION: ACTUAL

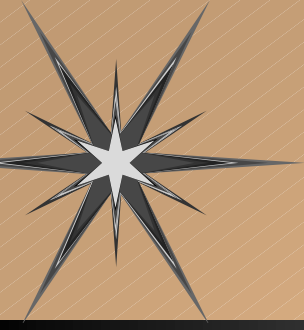




# LSST to LBT Comparison

Comparison of	LSST	and	LBT
Moving Mass	290		700 Metric tons
Crings	9 meters		14 meters
Pier Diameter	10.5 meters		14 meters

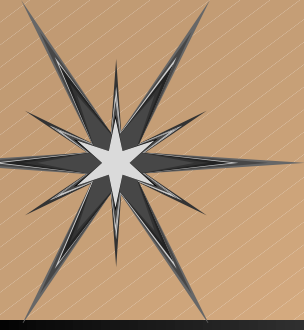




# We can build LSST

- LBT assembled in Milan.
- LSST is about half this size, we can easily build it.

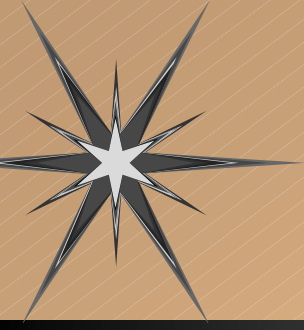




# LBT Acceptance Tests

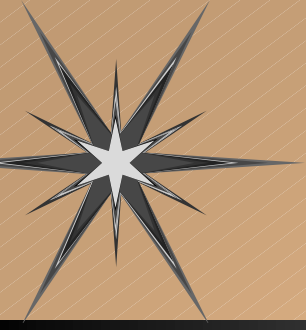
- LBT preliminary performance data with two of four motors on each axis.
  - Elevation resonant frequency 7hz
  - Azimuth resonant frequency 3hz and 10hz, The 3hz appears to be the electrical cabinet





# Mass and cost estimate

- Least Resonant Frequencies should exceed 10 Hz.
- LBT grew from 560 tons to 700 tons from design to construction so LSST should finish around 290 tons ( $290/700=.41$ ).
- Telescope Structure and Mechanics Cost 45% of LBT (21M) \$9.5 million .
- Telescope Structure and Mechanics Cost 170% of Magellan (6.1M) \$10.4 million .



# Tall Tent Poles

- Credibility----How can I convince you we can build an 8.4m telescope structure which has only 270 tons of moving mass, a 10hz resonant frequency and cost \$10 million.
  - We need detailed engineering studies.
  - Start design to show critical systems.
  - What does it take for YOU to believe it.